



Go Further

AVL



# OPTIMIERUNG DES ABSCHRECKENS BEI DER WÄRMEBEHANDLUNG VON AL-GUSSTEILEN MITTELS SIMULATION

## FORD

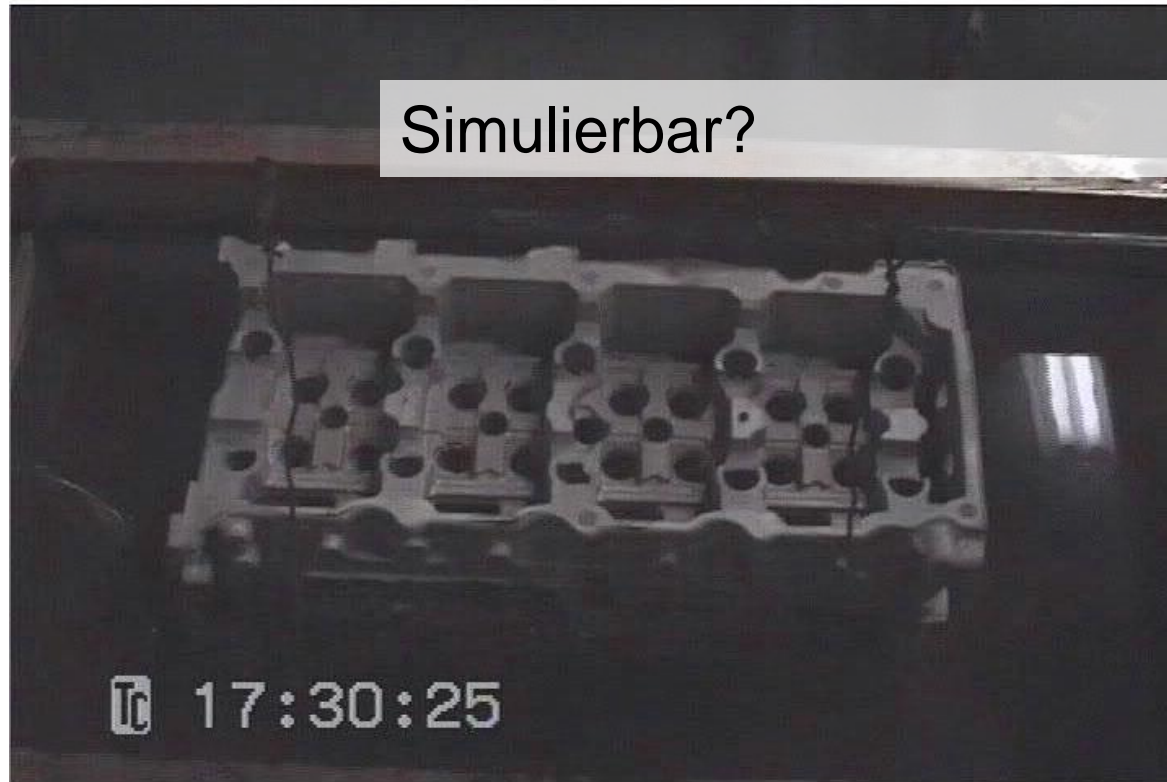
Aslihan Kaynar, James Jan, Ulrich Weiss

## AVL

David Greif, Rok Kopun

60. Österreichische Gießereitagung mit Fachausstellung  
7./8. April 2016, Bad Ischl, Austria

# COMPLEX AND CHAOTIC BOILING PROCESS



# EINFÜHRUNG PROBLEMSTELLUNG



## Problem:

- Rissbildung im Zylinderkopf
- Deformationen

## Mögliche Ursachen:

- Eigenspannungen aus dem Wärmebehandlungsprozeß
- Überlagerung von Betriebslasten
- Überbeanspruchung des Werkstoffs

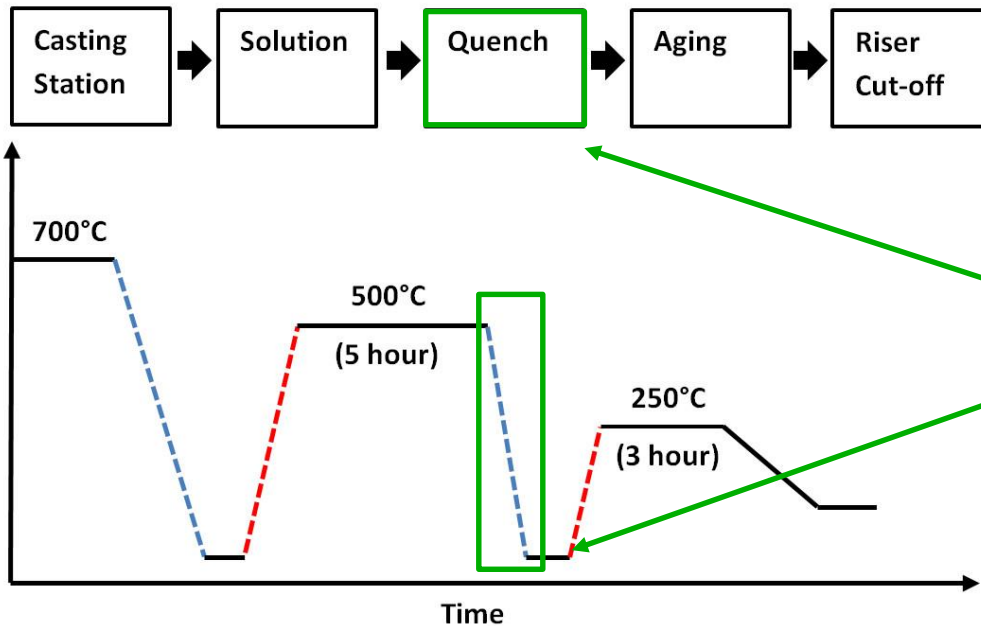
## Folgen:

- Leckage, Motorschaden

## Lösungsansatz:

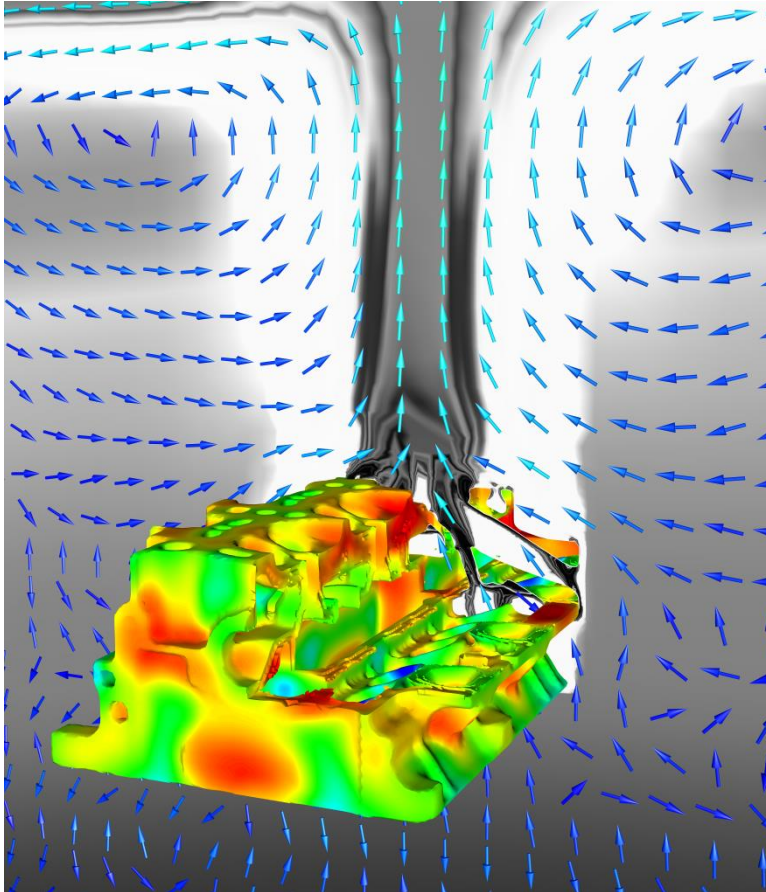
- Simulationsverfahren zur Bewertung der Eigenspannungen
- Reduktion der Eigenspannungen
- Optimierung der Wärmebehandlung

# SCHEMATISCHE WÄRMEBEHANDLUNG



## Wärmebehandlung für Aluminium-Gußteile

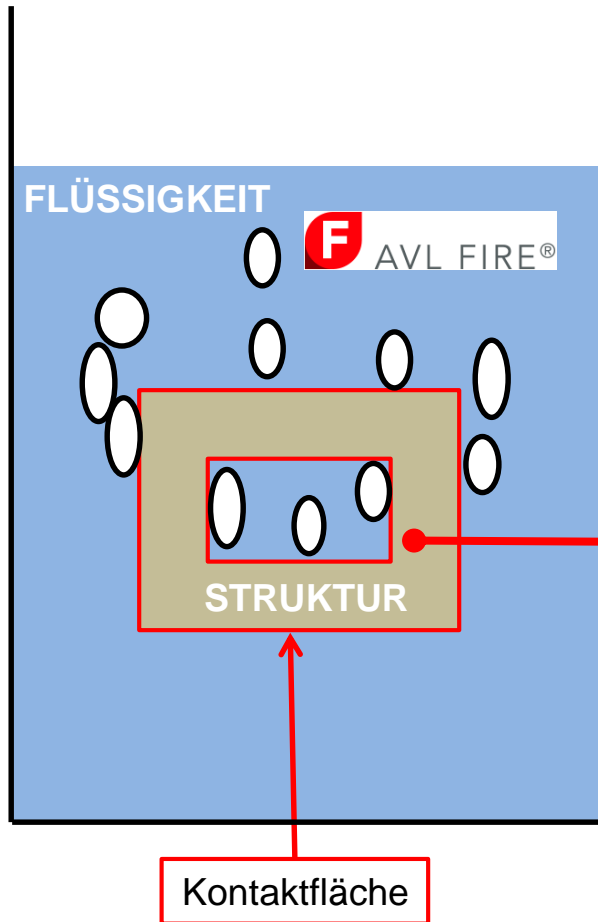
- Gießen
- Abkühlen
- Lösungsglühen bei ~500°C
- Abschrecken
- Auslagern (Altern) bei ~250°C
- Bearbeitung



## Simulation des Abschreckvorgangs

- Mit AVL FIRE™ können Luft- und Eintauchabschrecken sowie Sprayquenching simuliert werden
- Ermittlung des zeitlich aufgelösten Temperaturfelds im Bauteil infolge der Um- und Durchströmung und des Siedens an der Oberfläche
- Erzeugen von Eingabedaten für die Finite-Elemente-Analyse
- Ermittlung des Spannungs-Dehnungsfelds mit geeigneten Materialgesetzen in Abaqus
- Vorhersage der Bauteileigenspannungen
- Grundlage für die Bewertung von Prozeßparametern

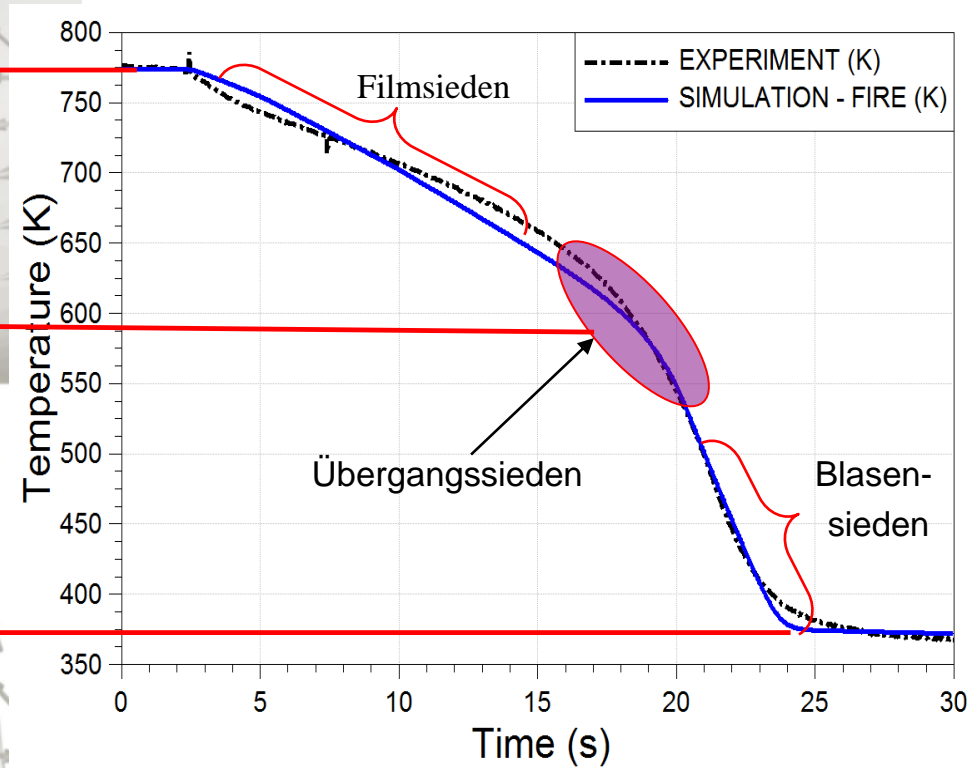
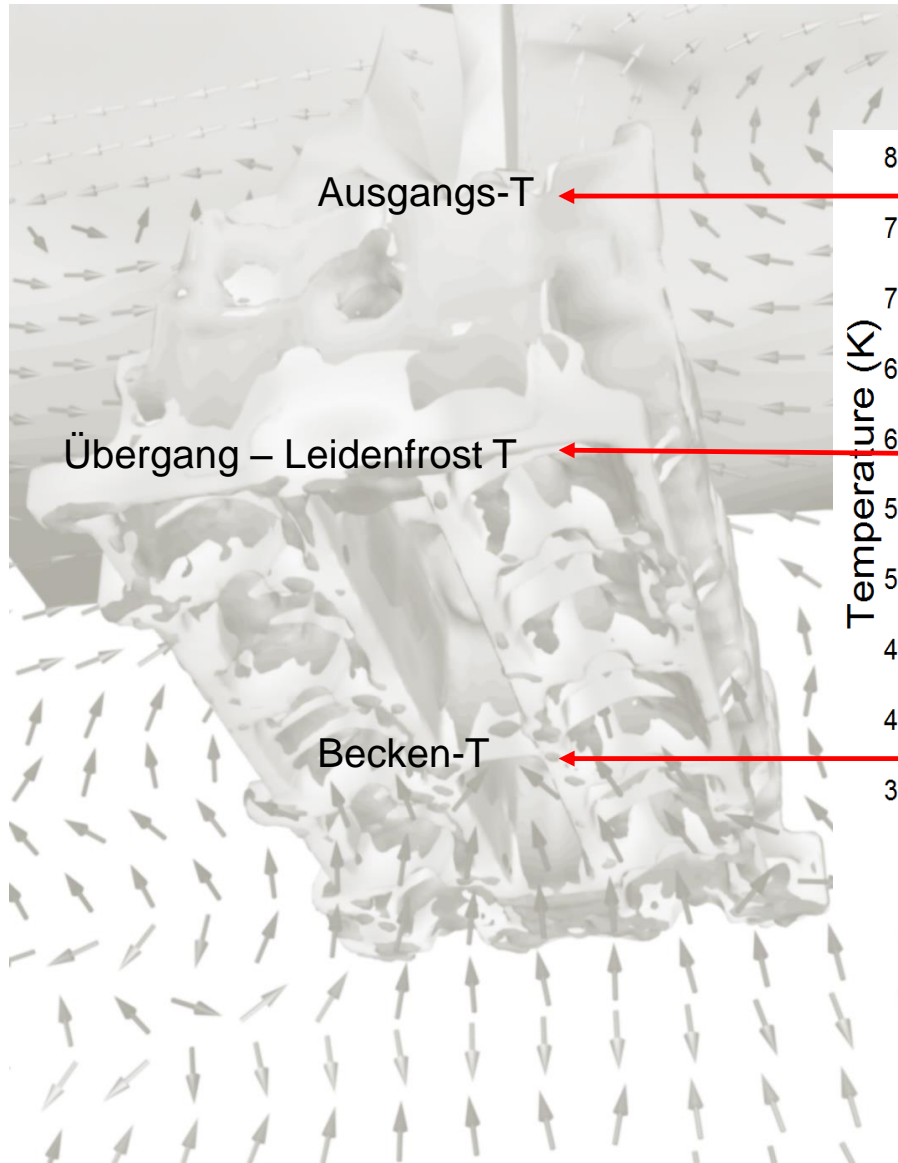
# SIMULATION DES ABSCHRECKVORGANGS



- CFD für Evaluierung der Temperatur in der Struktur
- Flüssigkeit und Struktur sind gekoppelt



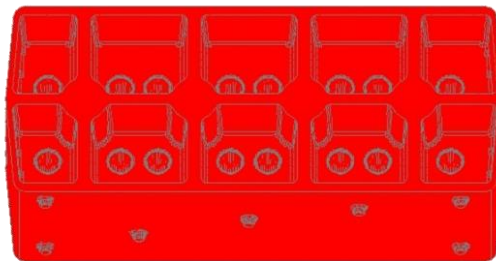
# MODELLIERUNG DES EINTAUCHABSCHRECKENS SIEDEPHÄNOMENE



# VALIDIERUNG TEST GEOMETRIEN

## Kooperation mit NEMAK

- Die Ergebnisse wurden im **FVV Projekt "Quench IT"** ermittelt und zur Validierung herangezogen
- Die Messungen wurden von Nemak als wichtigem Industriepartner durchgeführt
- Geometrie: mittlere Komplexität, realistische Baugröße und Wärmekapazität)



## Immersion Quenching Simulation of Realistic Cylinder Head Geometry

Rok Kopun  
AVL-AST d.o.o.

Dongsheng Zhang and Wilfried Edelbauer  
AVL LIST GmbH

Bernhard Stauder  
NEMAK Linz GmbH

Branislav Basara  
AVL LIST GmbH

David Greif  
AVL-AST d.o.o.

### ABSTRACT

In this paper, a recently improved Computational Fluid Dynamics (CFD) methodology for virtual prototyping of the heat treatment of cast aluminum parts, above most of cylinder heads of internal combustion engines (ICE), is presented. The comparison between measurement data and numerical results has been carried out to simulate the real time immersion quenching cooling process of realistic cylinder head structure using the commercial CFD code AVL FIRE®. The Eulerian multi-fluid modeling approach is used to handle the boiling flow and the heat transfer between the heated structure and the sub-cooled liquid. While for the fluid region governing equations are solved for each phase separately, only the energy equation is solved in the solid region. Heat transfer coefficients depend on the boiling regimes which are separated by the Leidenfrost temperature. The objective of the present research work is to present an update of the quenching model where

### Referenz:

Kopun, R., Zhang, D., Edelbauer, W., Stauder, B. et al., "Immersion Quenching Simulation of Realistic Cylinder Head Geometry," *SAE Int. J. Mater. Manf.* 7(3):520-529, 2014, doi:10.4271/2014-01-0641.

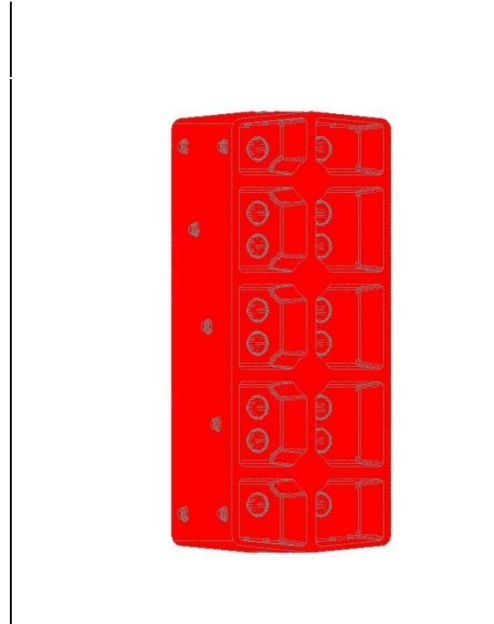


# CFD SIMULATIONSERGEBNISSE VALIDIERUNG

- Horizontale Eintauchrichtung



- Vertikale Eintauchrichtung

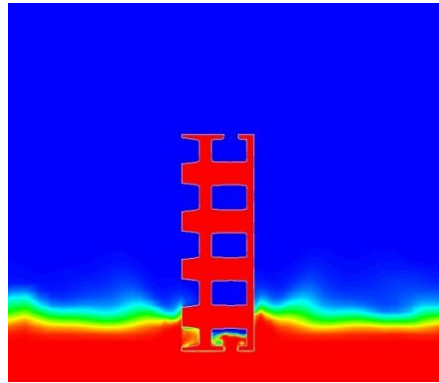


Aluminium  
L×B×H = 400×170×140 mm  
Representatives Gewicht

2014-01-0641  
Published 04/01/2014  
Copyright © 2014 SAE International  
doi:[10.4271/2014-01-0641](https://doi.org/10.4271/2014-01-0641)

# CFD SIMULATIONSERGEBNISSE VALIDIERUNG

Time: 1 sec

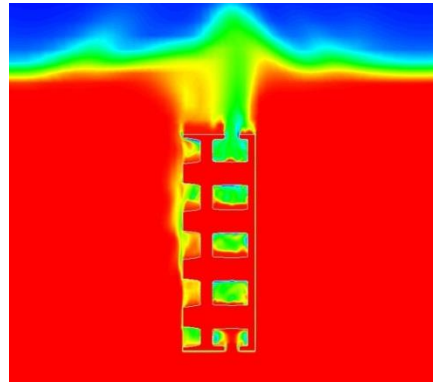


Volume fraction

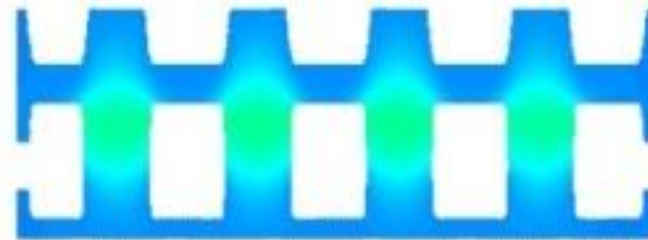
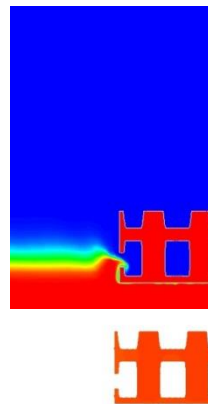


Temperature

Time: 5 sec

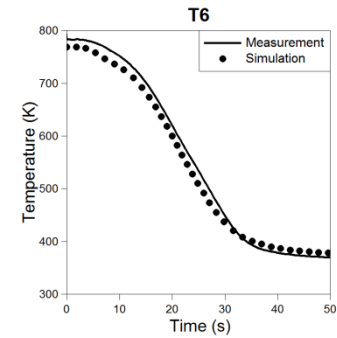
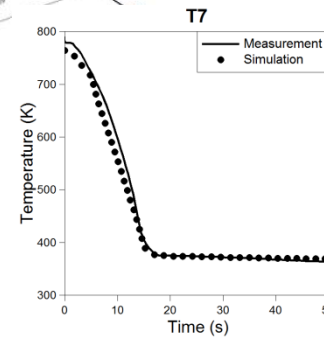
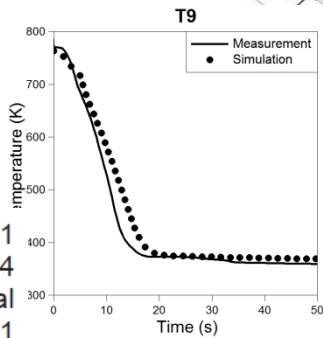
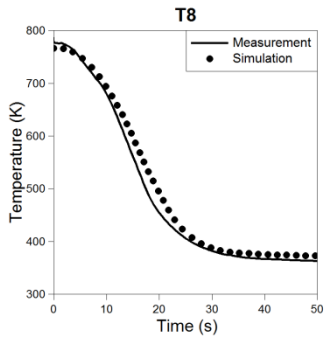
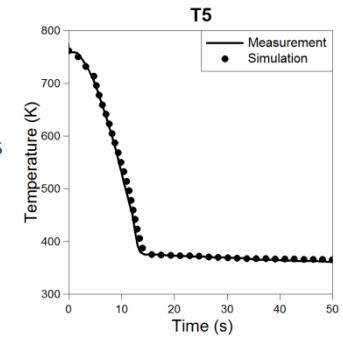
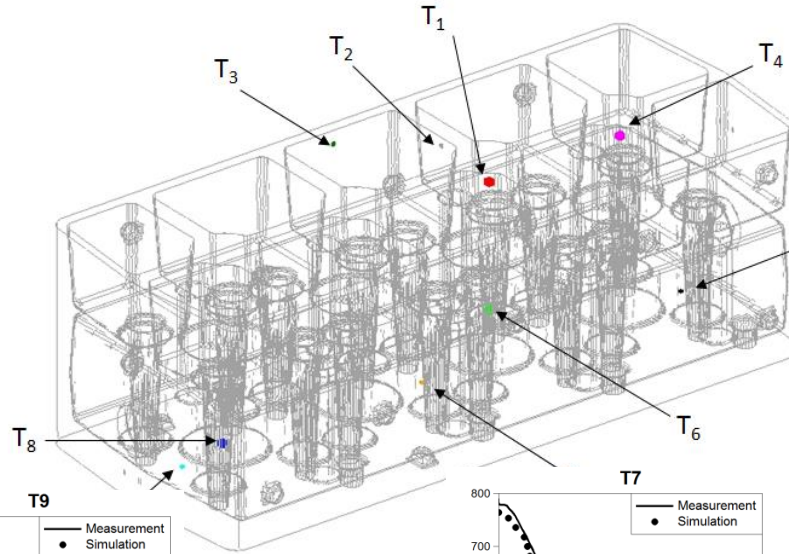
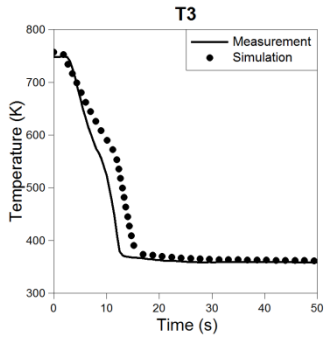
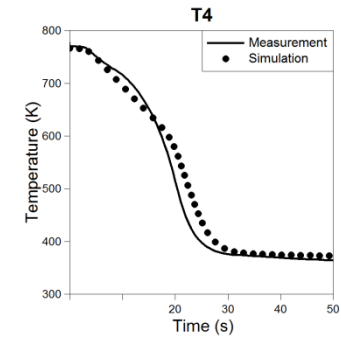
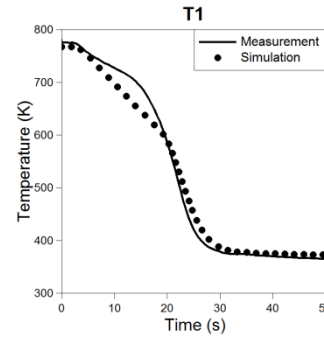
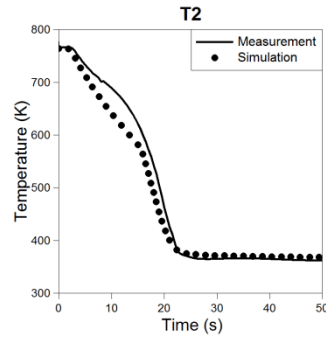
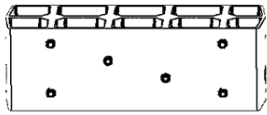


Time: 30 sec



# CFD SIMULATION RESULTS VALIDIERUNG

## Horizontal



2014-01-0641

Published 04/01/2014

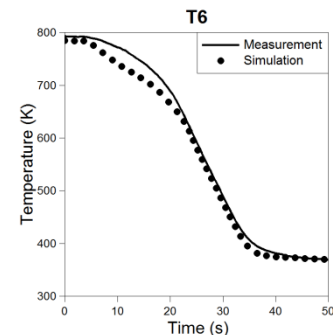
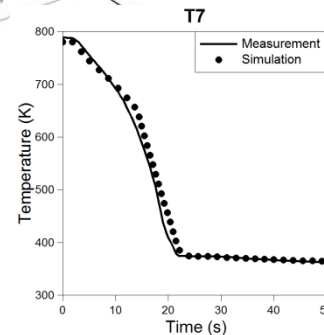
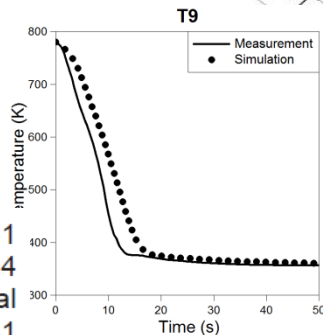
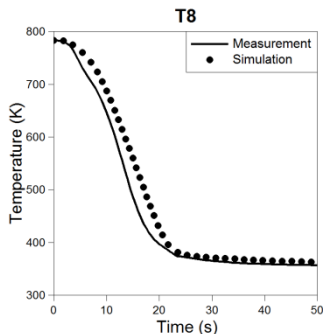
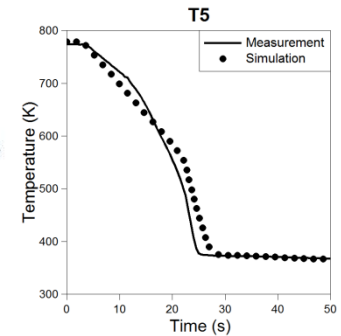
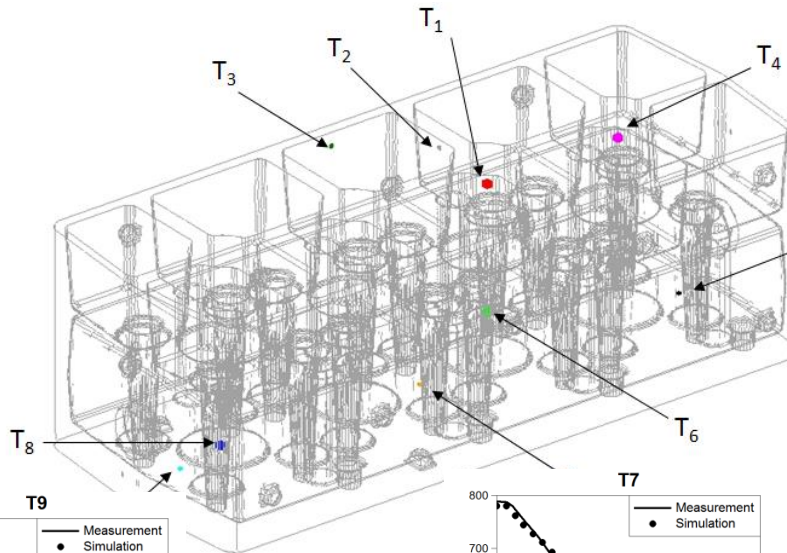
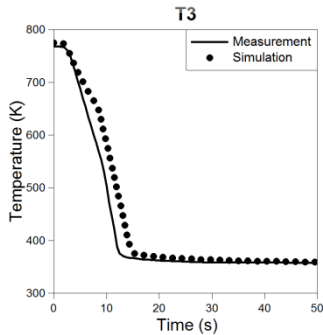
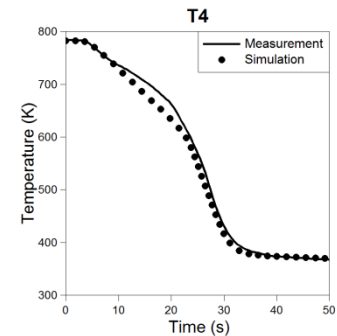
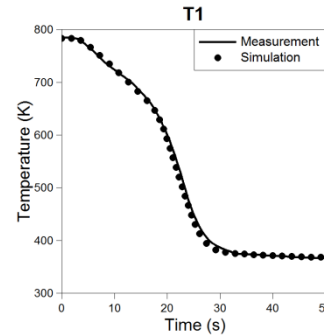
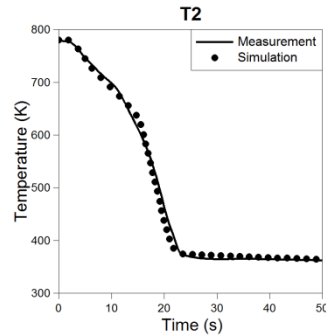
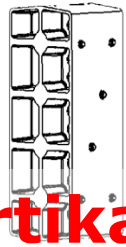
Copyright © 2014 SAE International

doi:10.4271/2014-01-0641

internal | Public | Confidential

# CFD SIMULATION RESULTS VALIDIERUNG

Vertikal



2014-01-0641

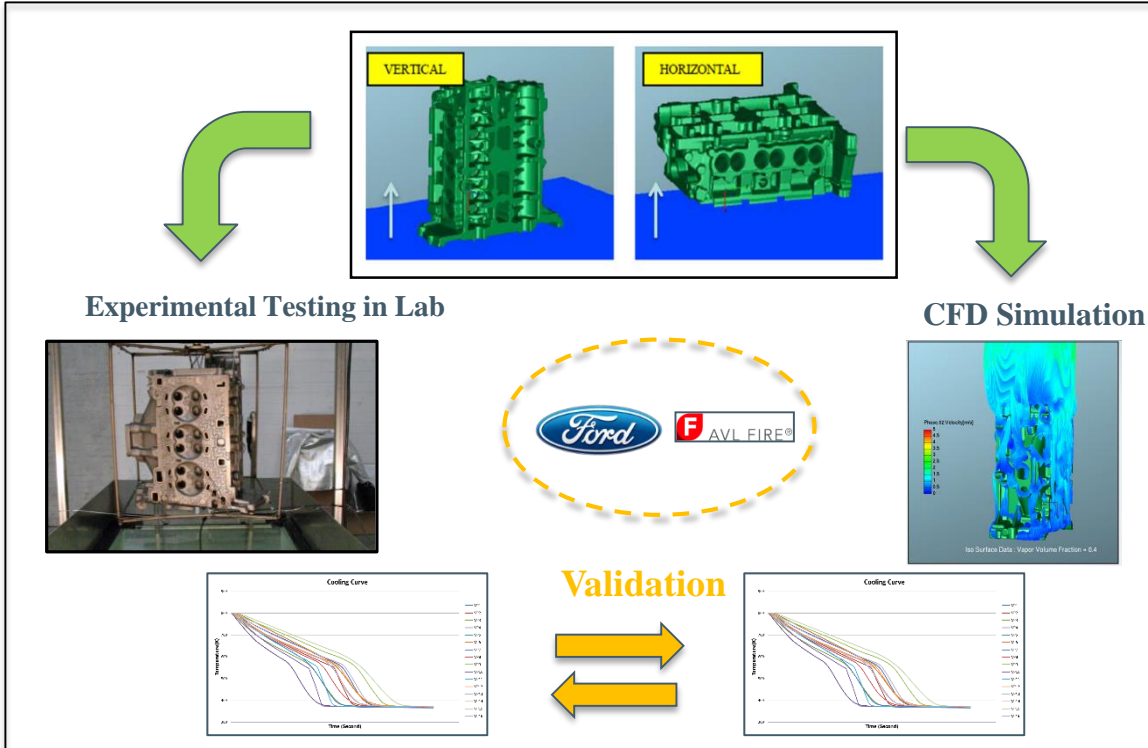
Published 04/01/2014

Copyright © 2014 SAE International

doi:10.4271/2014-01-0641

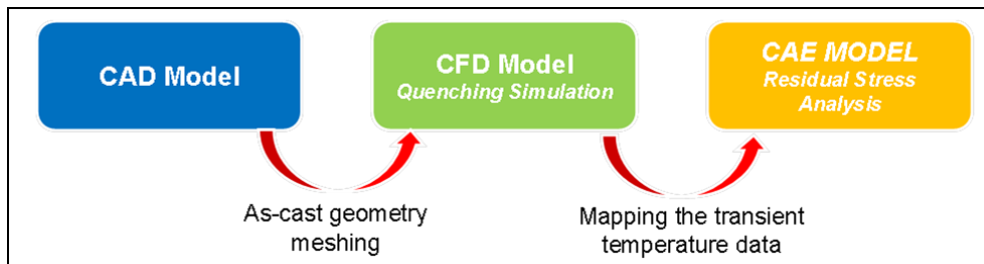
internal | Public | Confidential

# OBJECTIVE



Ford's requirement is a **physical modeling CAE** method to capture transient temperature distribution during quenching.

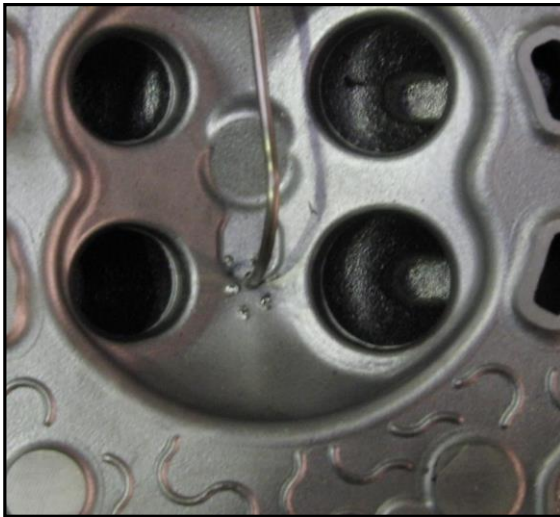
- Software Requirements**
- ✓ Correlation
  - ✓ Predictability
  - ✓ Compatibility



Providing transient temperature data for CAE model

# EXPERIMENT - THERMOCOUPLES

- Prototype cylinder heads : **as-cast, not cubed, non-heat treated condition**
- Drilling thermocouple holes (CNC)
- "**Embedded and peened**" method
- Sealing with a **ceramic paste** for the quenching experiments

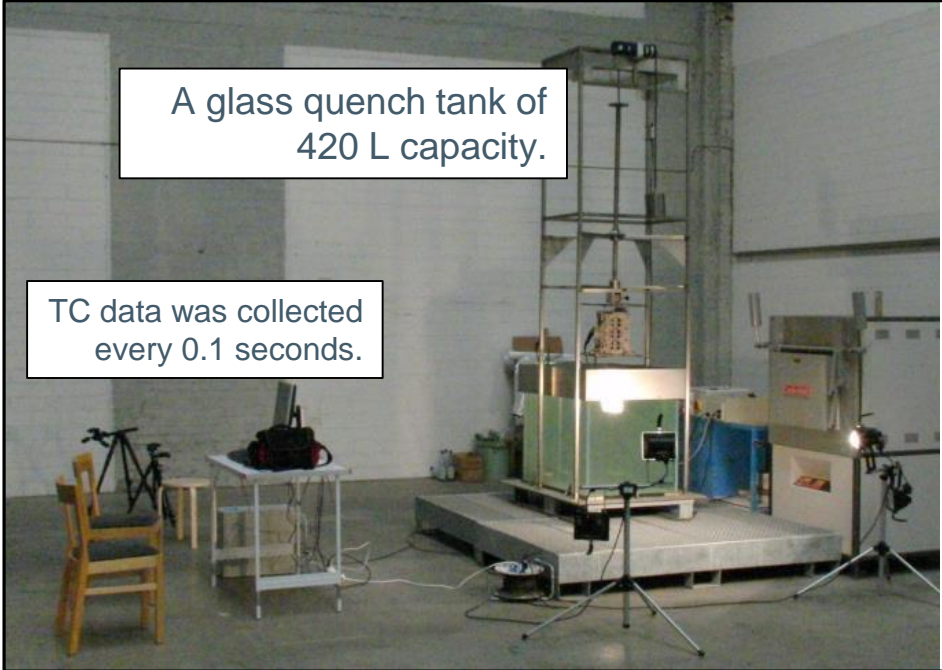


*Embedded and Peened Thermocouple  
(combustion chamber roof location)*



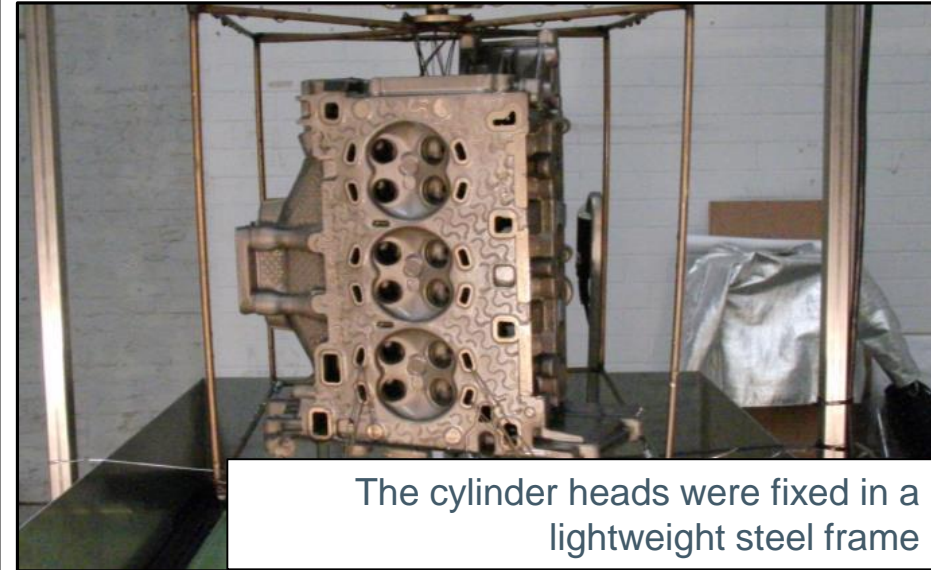
*Thermocouple Locations*

# EXPERIMENTAL STUDY




A glass quench tank of 420 L capacity.

TC data was collected every 0.1 seconds.

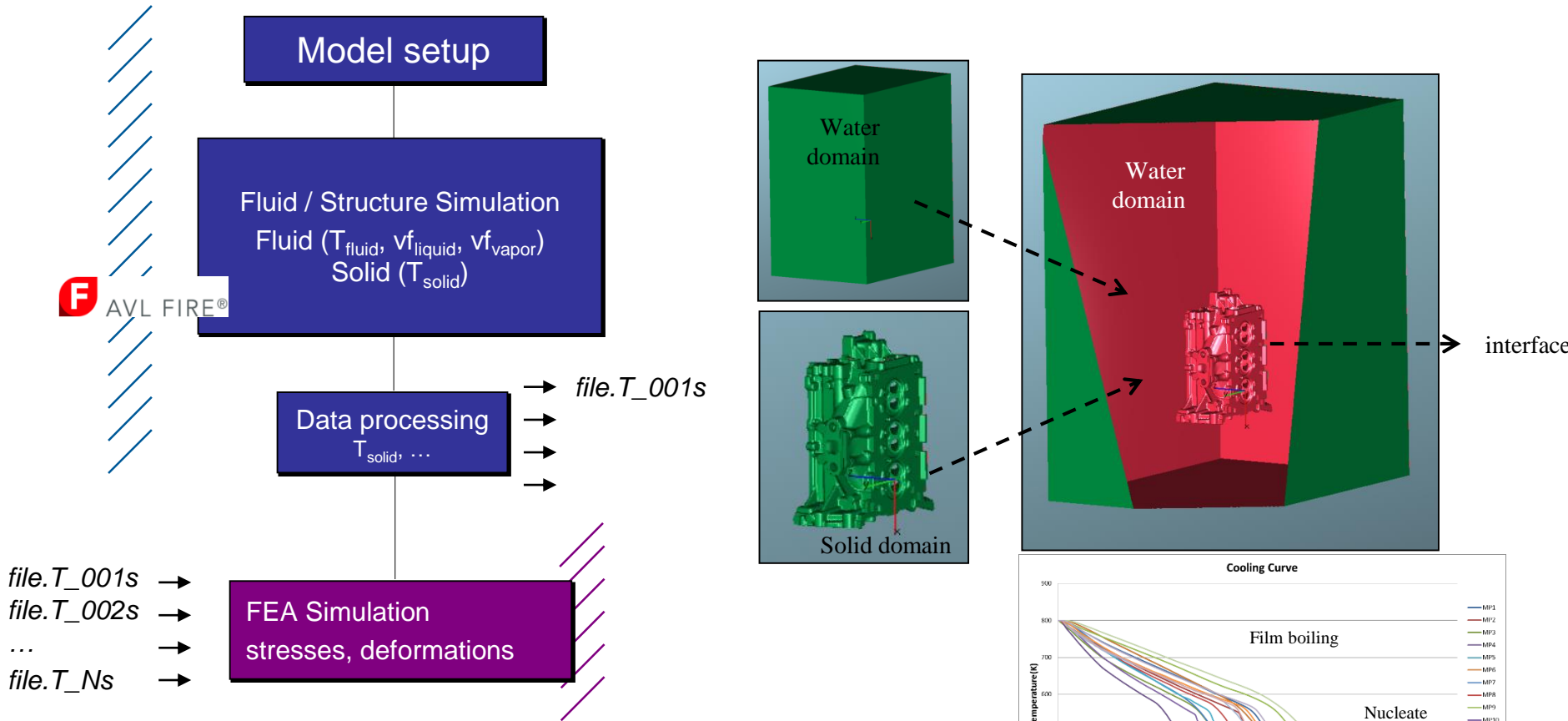


|                 |     |
|-----------------|-----|
| Temperature     | °C  |
| Solutionization | 527 |
| Quenchant       | 91  |



Recordings were taken with a rate of 300 frames per second, resulting in a slow motion mode of 1:10 when using standard viewers.

# COMPUTATIONAL APPROACH



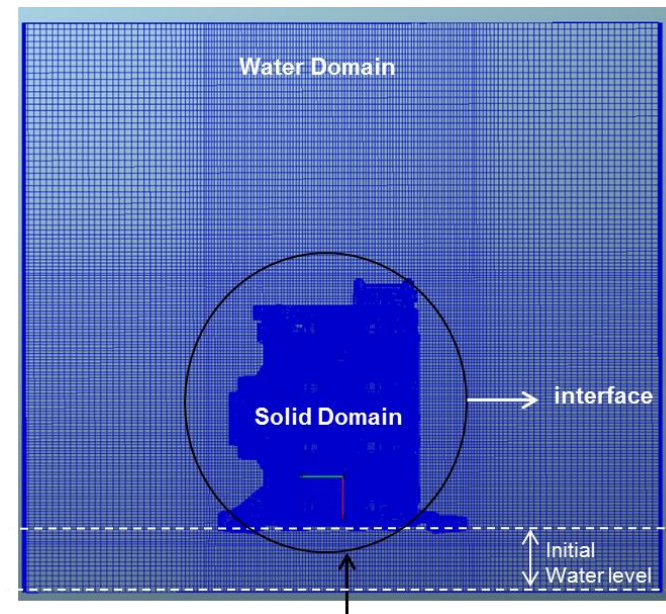
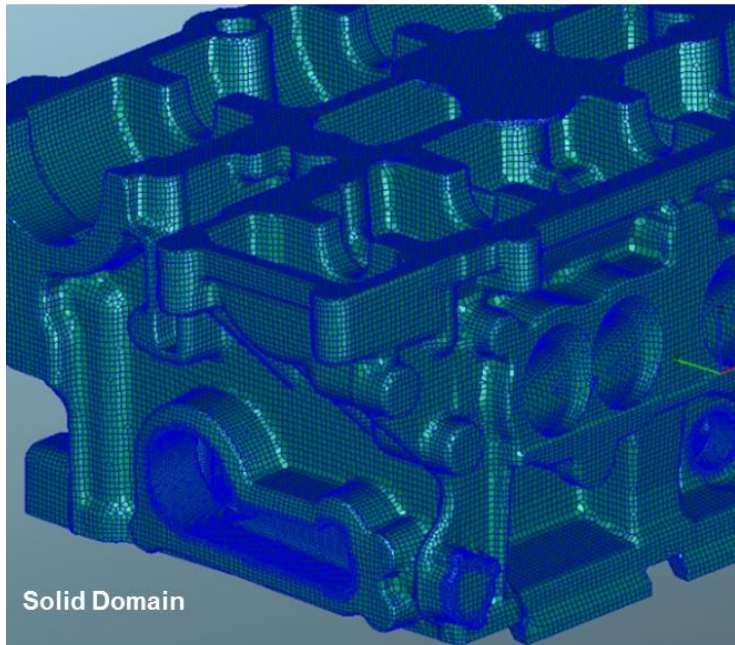
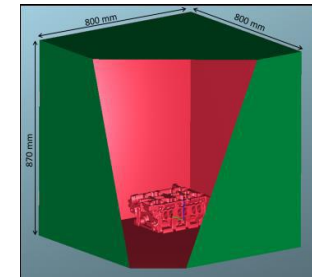
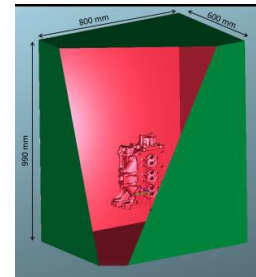
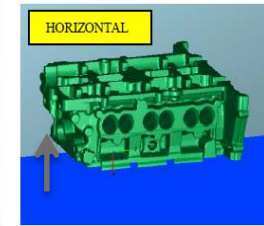
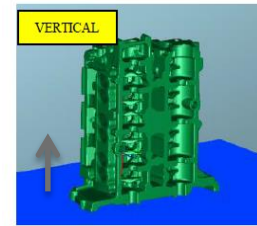
Transient temperature distribution to be used as input for stress analysis



# COMPUTATIONAL MODEL



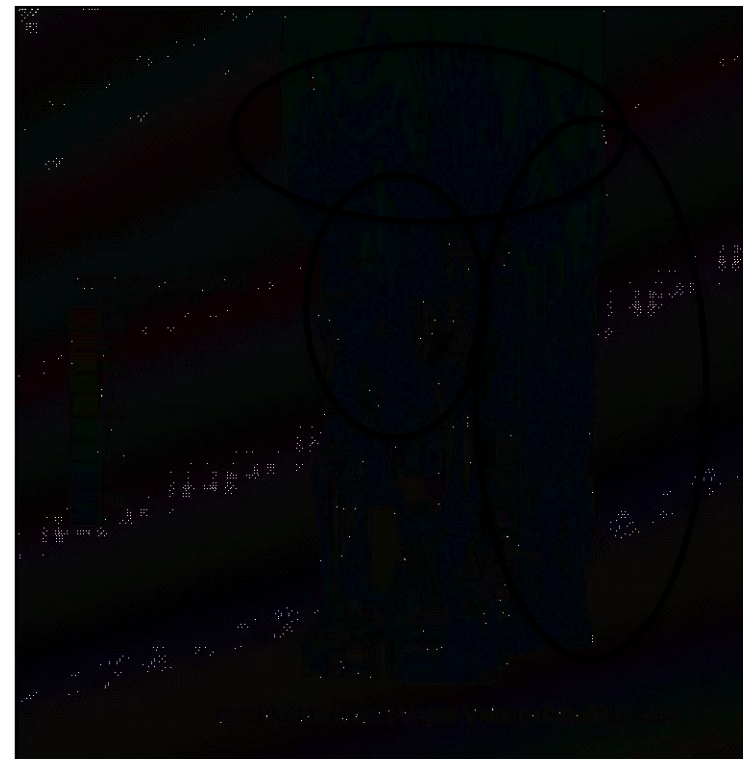
| Simulation Parameters     |                        |
|---------------------------|------------------------|
| Solid & Water Temperature | Similar as experiments |
| Inlet Boundary Condition  | Velocity Inlet         |
| Submerging speed          | 0.7 m/s                |
| Outlet Boudnary Condition | Pressure Outlet        |
| Forced flow               | No                     |



# VAPOR FORMATION VERTICAL ORIENTATION

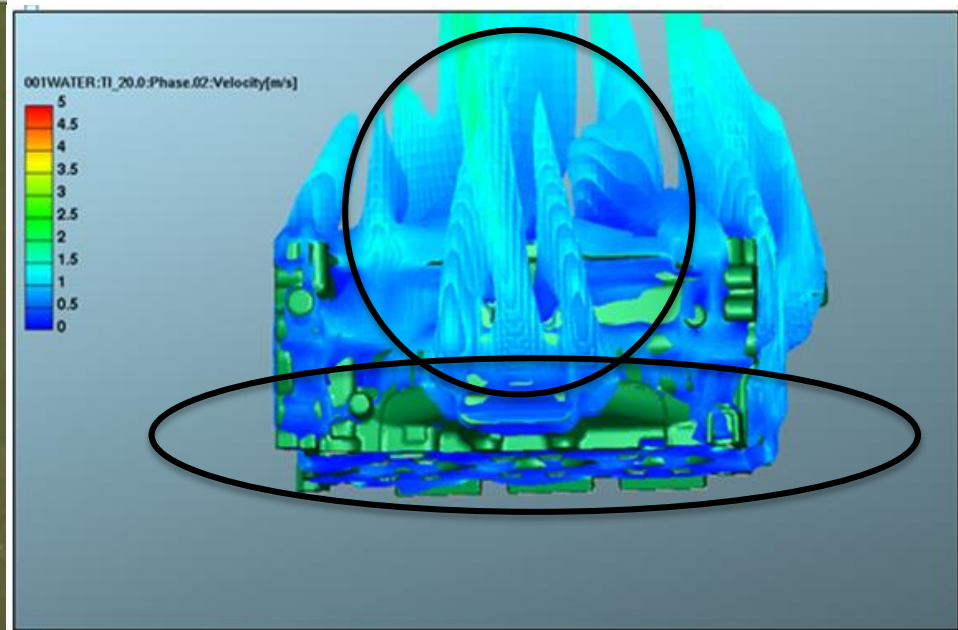


## Experiment vs. CFD



# VAPOR FORMATION HORIZONTAL ORIENTATION

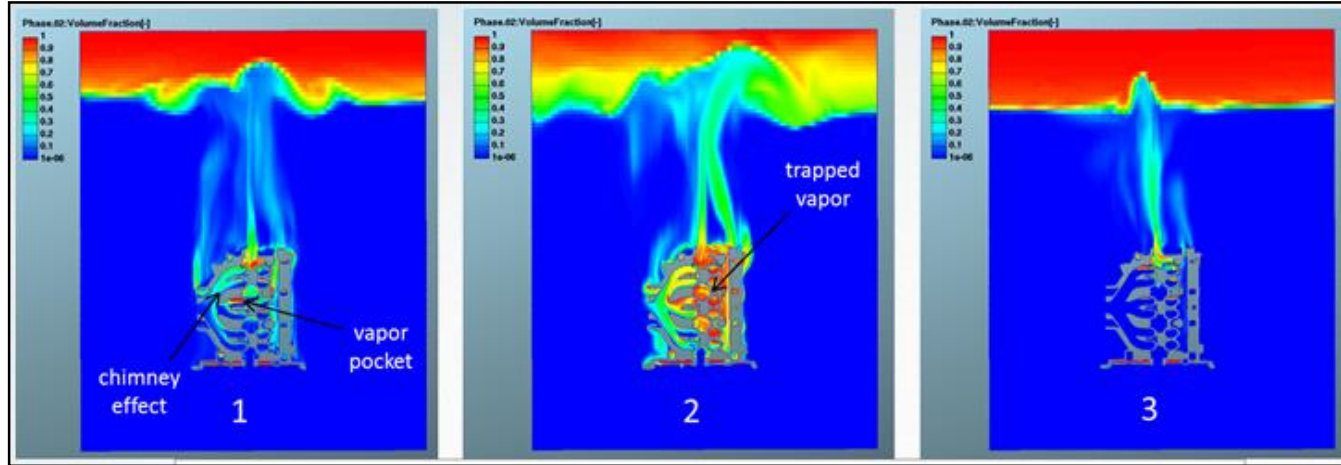
## Experiment vs. CFD



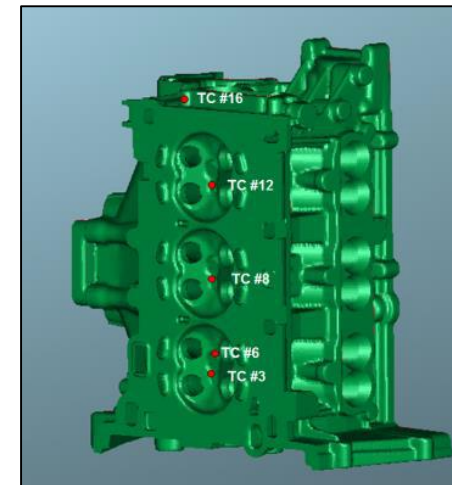
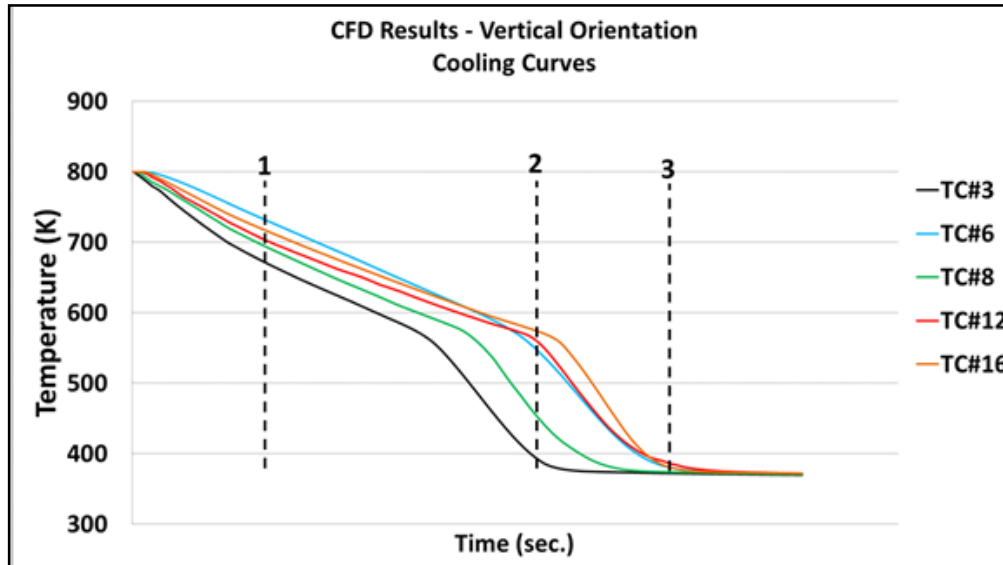
Good correlation in terms of vapor formation!

# VAPOR FORMATION & TEMPERATURE VERTICAL ORIENTATION

Vapor Volume Fraction distribution on a plane section for three boiling regimes.(1,2,3)

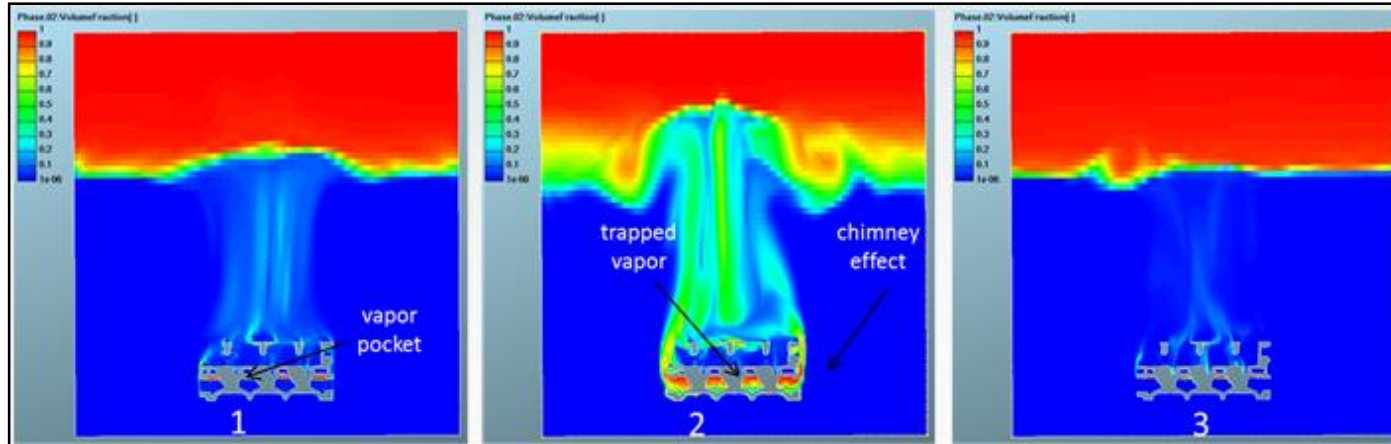


Temperature history data for each monitoring point in vertical orientation.

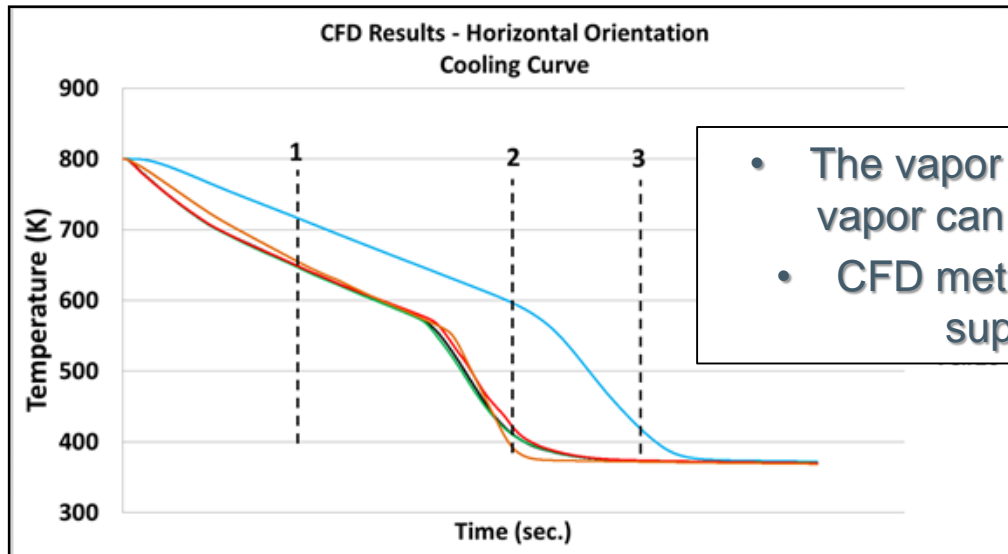


# VAPOR FORMATION & TEMPERATURE HORIZONTAL ORIENTATION

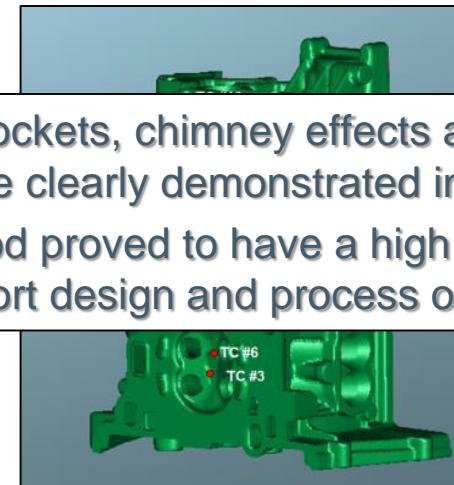
Vapor Volume Fraction distribution on a plane section for three boiling regimes.(1,2,3)



Temperature history data for each monitoring point in horizontal orientation.



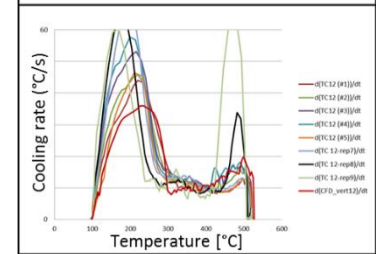
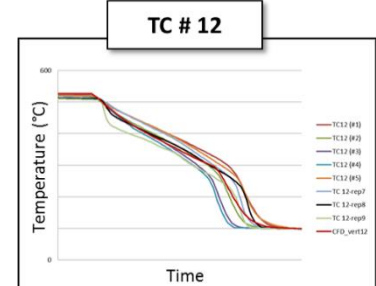
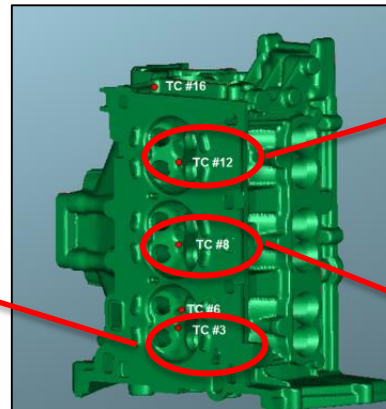
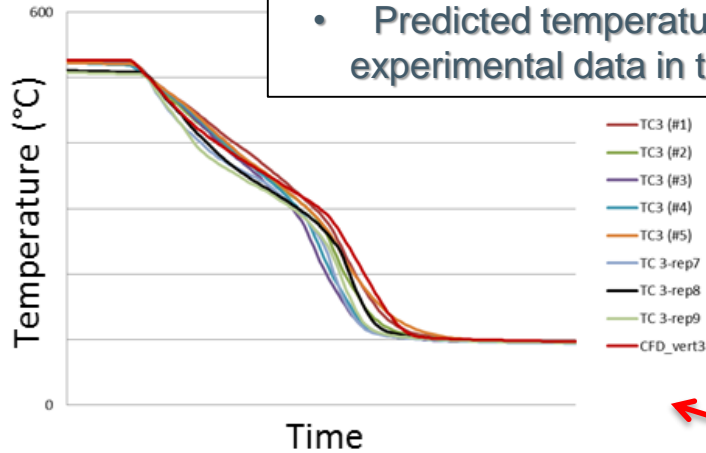
- The vapor pockets, chimney effects and trapped vapor can be clearly demonstrated in simulation
- CFD method proved to have a high potential to support design and process optimization.



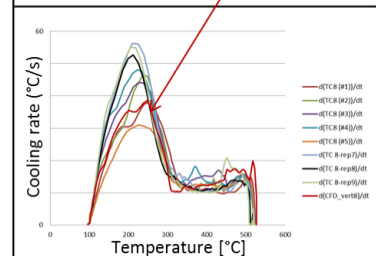
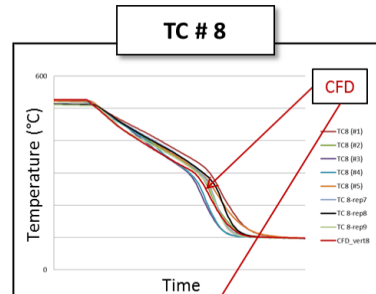
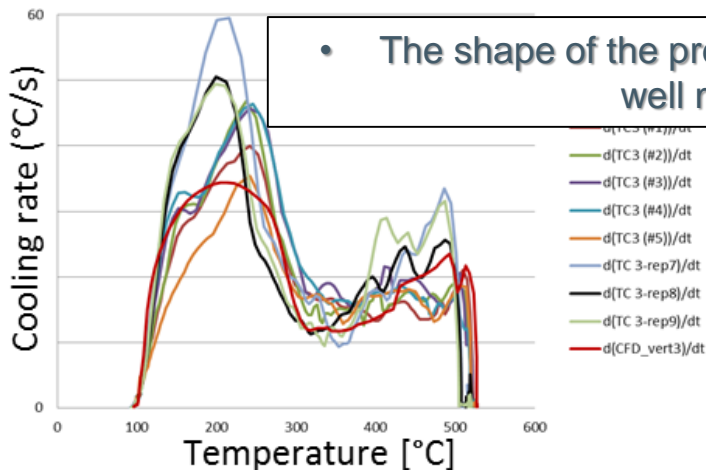
# RESULTS – EXPERIMENT VS. CFD

## TC # 3

- Predicted temperature history: good agreement with the experimental data in the film and transition boiling regime

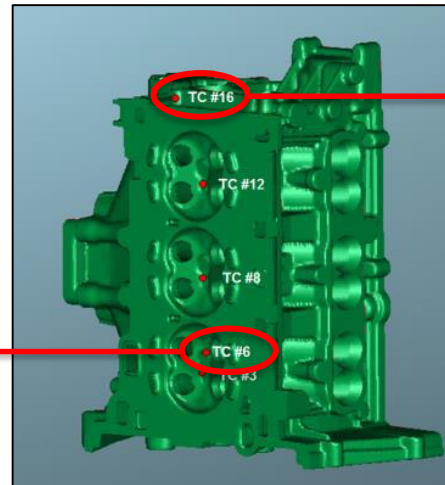
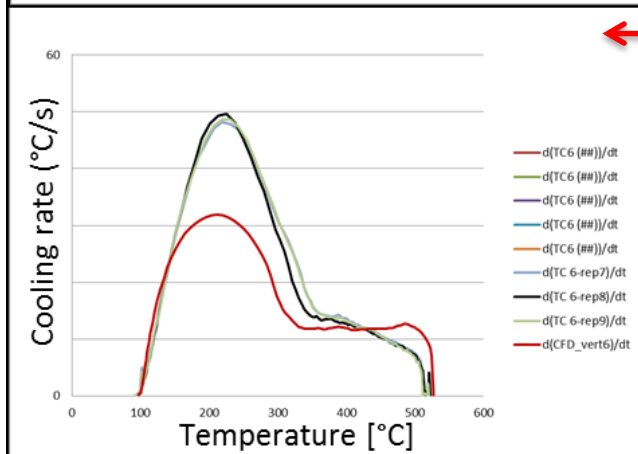
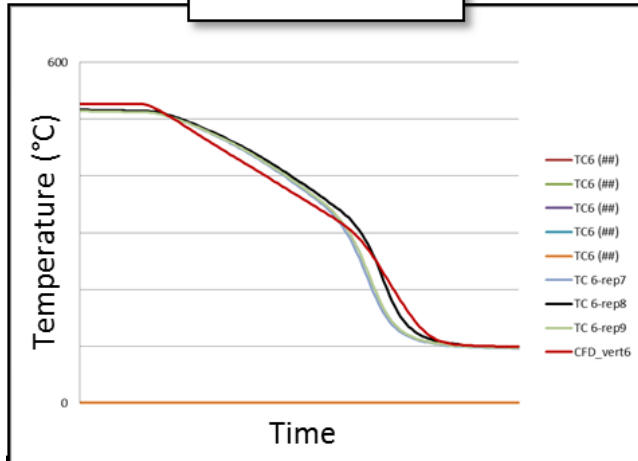


- The shape of the predicted cooling rate graphs are also well matching with the experimental data

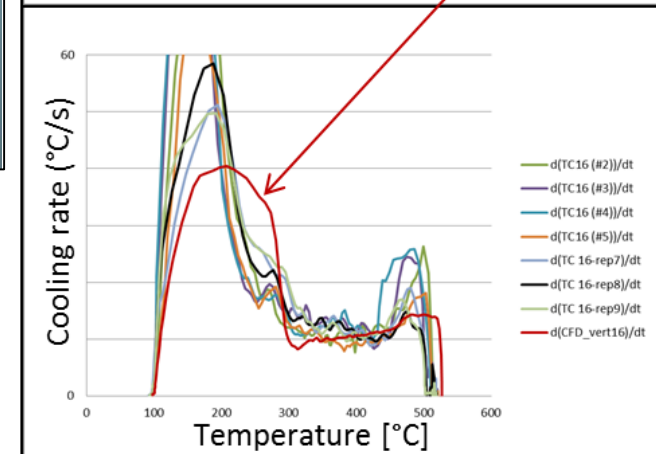
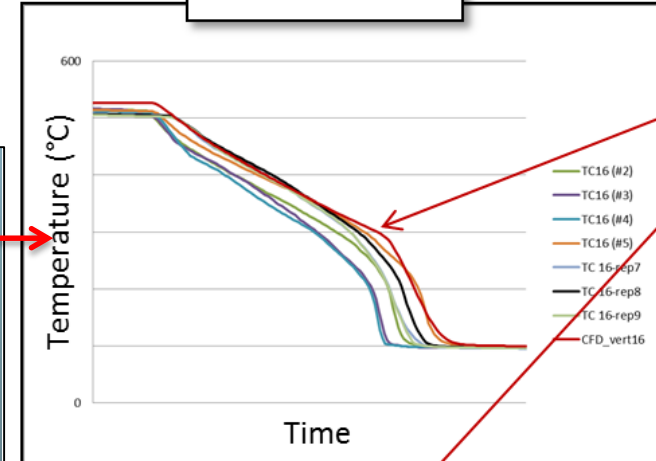


# RESULTS – EXPERIMENT VS. CFD

## TC # 6



## TC # 16



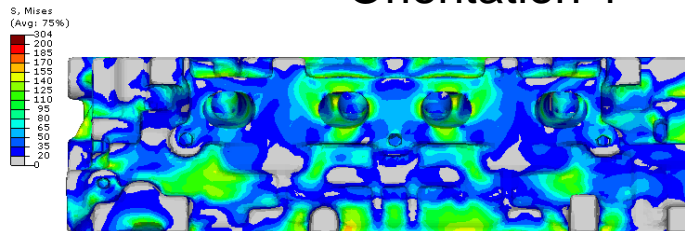
CFD

# STRESSES AND DEFORMATIONS

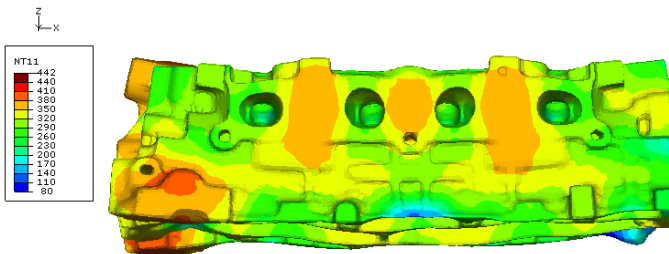
## Effect of submerging direction

Orientation 1

Stress

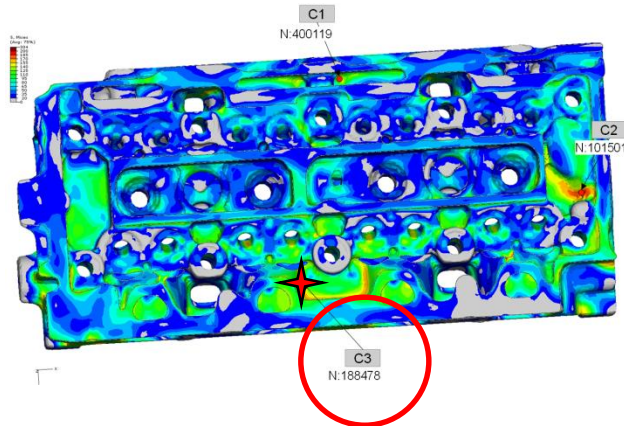


Temperature and deformation





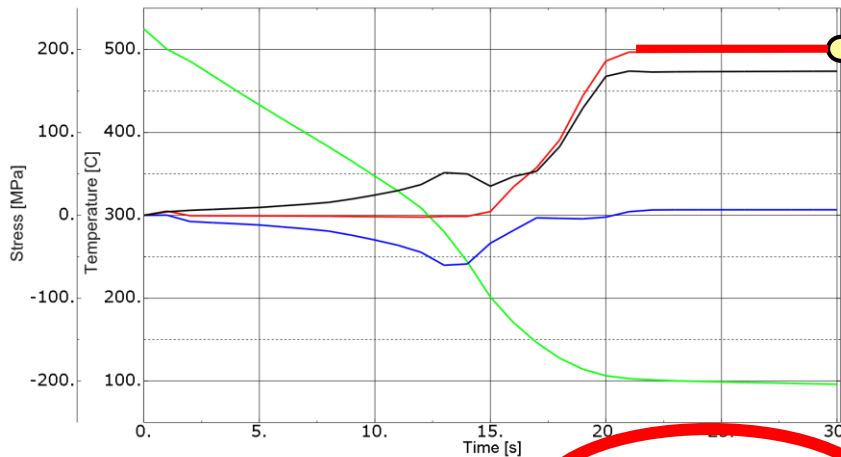
# DIRECT QUENCHING STRESSES AND DEFORMATIONS (FEA)



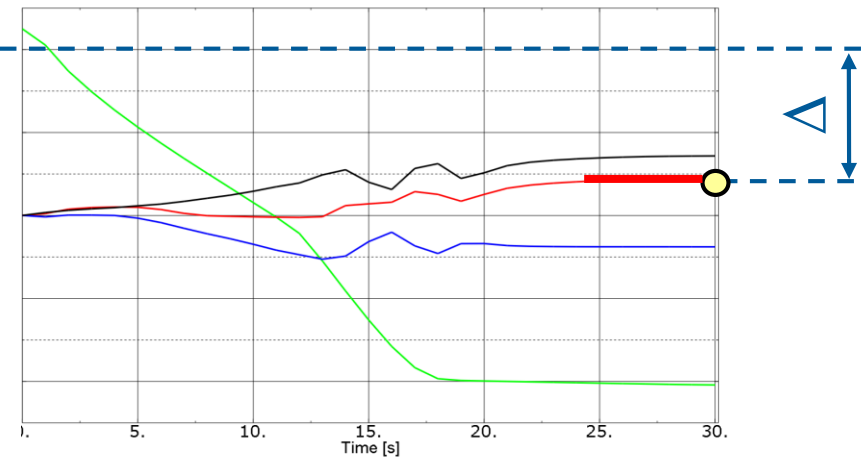
## Evaluation point C3

- Tensile stress dominant
- Orientation I > Orientation II

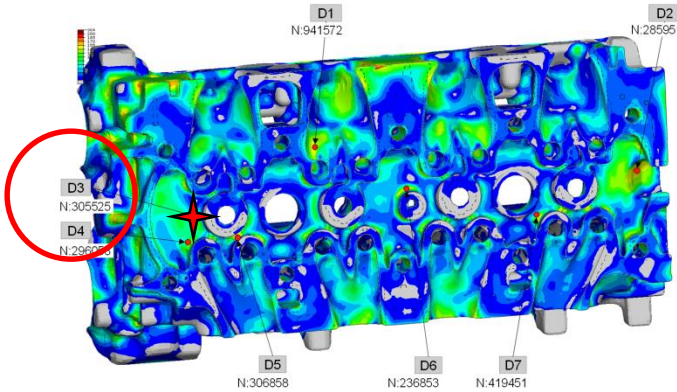
Orientation I



Orientation II



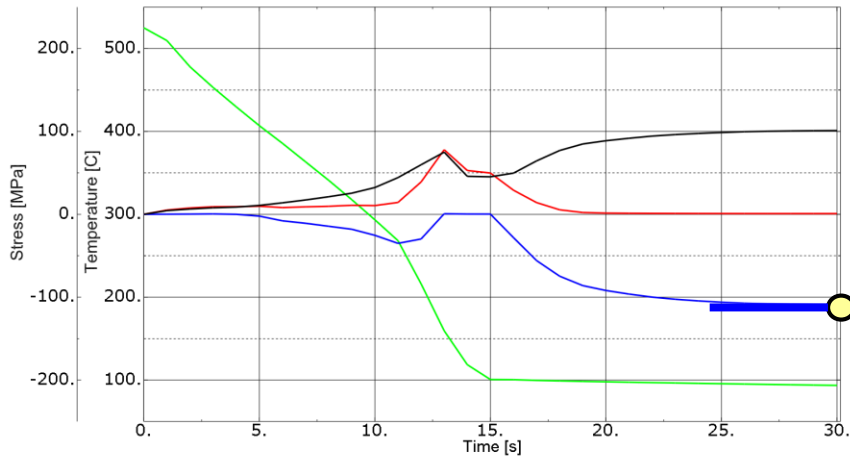
# DIRECT QUENCHING STRESSES AND DEFORMATIONS (FEA)



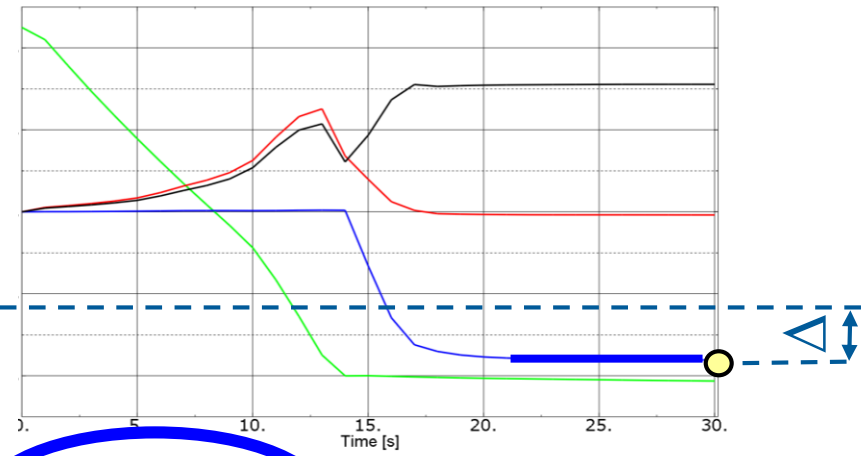
## Evaluation point D3

- Compressive stress dominant
- Orientation I < Orientation II

### Orientation I



### Orientation II



## ZUSAMMENFASSUNG

- Die Simulation des Eintauchabschreckens mit AVL FIRE liefert realistische zeitaufgelöste Temperaturfelder, die die nachgeschaltete FE-Simulation der Eigenspannungen ermöglichen.
- Das Modell der Variablen Leidenfrosttemperatur erhöht die Aussagefähigkeit erheblich.
- Das Verfahren wird bereits erfolgreich bei der Beurteilung des Abschreckprozesses von Zylinderköpfen eingesetzt.
- Das vorgestellte Simulationsverfahren bietet ein wertvolles Werkzeug, um simulatorisch ohne Versuche und Messungen Bauteileigenschaften vorhersagen zu können, die durch das Abschrecken verursacht werden.

VIELEN DANK



[www.avl.com](http://www.avl.com)

[david.greif@avl.com](mailto:david.greif@avl.com)